

Influence of Quality Parameters on Quantities of Pushover Analysis Results

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Abstract: Pushover analysis is being extensively used for design and performance evaluation of structures under seismic loads. Generation of pushover curve from the analysis of RC structures involves a tremendous amount of computational efforts and analysis results are very sensitive to techniques employed for geometric and material modelling. This analytical investigation presents the influence of variation in materials strengths, effective cover to reinforcement variations and sequence of plastic hinge formations on pushover analysis results in performance evaluation of earthquake resistant design. A single bay single storey RC frame is considered in the present study.

Keywords: Performance based design; Seismic assessment; Geometric modelling; Material modelling; Pushover analysis.

Introduction

Pushover Analysis has been widely used as a tool to gauge the expected performance of a structural system by estimating its strength and deformation capacity in seismic design by means of static inelastic analysis. It is supported by three key concepts: capacity, demand and performance. The capacity is delineated by the capacity curve which shows the structure's capacity to withstand incremental lateral loading. Demand is indicated by the target displacement, representing the maximum displacement that may be expected by the structure during a considered ground motion and, intersection of capacity and demand is portrayed as performance. Based on the FEMA 356 and ATC 40 guidelines, pushover analysis is carried out. Geometric and material modelling capabilities in pushover analysis have been greatly enhanced by techniques that have been redefined and refined to be as close to reality as possible.

Review of Pushover Analysis – State of the Art

The work of Takeda and Sozen[1] where a realistic conceptual model for predicting the dynamic response of a reinforced concrete member has been studied based on a static force displacement relationship which reflects the changes in stiffness for loading and unloading of member is regarded as pioneering in the use of inelastic static analysis. Assumptions that a single mode is dominant and its shape is constant throughout the analysis was proposed and applied in pushover analysis by Gulkan and sozen[2]. Investigations by Helmut Krawinkler and Seneviratna [3] suggested that, a carefully performed pushover analysis would provide great insights to structural aspects that control seismic performance. A response spectrum based pushover procedure was proposed by A.S.Moghdam et al,[4] to obtain seismic response estimates on three types of asymmetrical buildings systems. Chopra and Goel [5] presented modal pushover analysis procedure for estimation of seismic demand and demonstrated the techniques accuracy and practical utility.

Influence of axial load ratio and loading path on plastic hinge length has been investigated by Li Peng and Yi Weijian [6]. Study by P.Poluraju et al [7] indicated that improperly designed and detailed RC frames with strong column weak beams, most of the hinges form in beams and columns have few hinges at limited damage levels. Seismic performance of 5 storied RC residential building according to Moroccan seismic code RPS2000 provisions assessed by M. Mouzzoun et al [8] indicated that the buildings could sustain moderate earthquakes but would be vulnerable to severe earthquake. Sensitivity of pushover curve to material and geometric modelling by comparing the analysis results with that of experimental investigations has been studied by Neena Panandikar (Hede), K.S. Babu Narayan [9].

Wide and varying research attempts to understand structural behavior and to make analysis design, detailing, monitoring and control of structural performance under seismic loads show the tremendous scope and need for refinement of unresolved issues.

This paper presents by the way of illustrations the effect of quality parameters variations like strength of concrete, steel strength, effective cover to reinforcement and variation in sequence of formation of plastic hinge on pushover analysis results and highlights the need for inclusion of sequence of plastic hinge formations in obtaining more meaningful and reliable results.

Details of RC frame subjected to pushover analysis parametric studies

A single bay single storey RC frame as shown in figure 1 is considered for analysis. The reinforcement details and cross sections of the beam and columns have been provided in figure 1b. Commercially available SAP2000 (version-14) has been used as the general finite element software for modelling and analysis. The graphical user interface has been used to create the material and geometric model and properties have been defined accordingly. M3 hinges have been considered as moment effects are predominant in all elements.

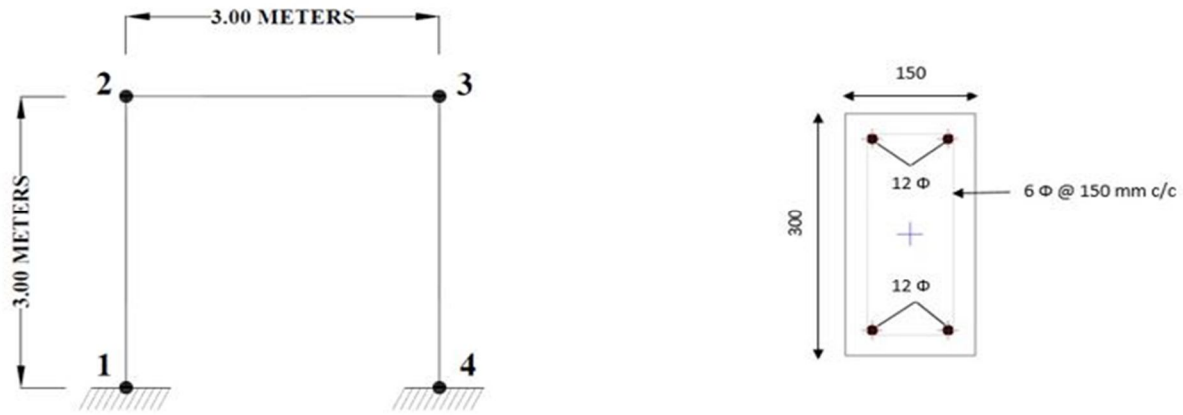


Figure 1. Details of single bay single storey RC frame

Analysis Results and Discussions

Effect of variation in material strengths and detailing on pushover analysis results

To show the influence of material strength and effective cover variations, pushover analysis is carried out on RC frame wherein five values of steel strength (f_s) (350,380,415,445,475 MPa), five values of concrete strength (f_c) (17, 18.5, 20, 21.5 and 23 MPa) and effective cover (d_c) (25, 30, and 35) central being adopted in design, higher and lower values accounting for 15% variations have been considered. Analysis results have been presented in Tables 1 to 3.

Table 1.Pushover Analysis Results for Effective Cover 25mm

| f_c f_s | 17 | | 18.5 | | 20 | | 21.5 | | 23 | |
|----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|
| | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) |
| 350 | 0.018716 | 43.294 | 0.018507 | 43.384 | 0.018323 | 43.467 | 0.018069 | 43.526 | 0.018008 | 43.619 |
| 380 | 0.019138 | 46.937 | 0.018941 | 47.078 | 0.018741 | 47.171 | 0.018561 | 47.259 | 0.018399 | 47.342 |
| 415 | 0.038578 | 51.006 | 0.01943 | 51.223 | 0.019227 | 51.461 | 0.019033 | 51.579 | 0.018856 | 51.672 |
| 445 | 0.03914 | 54.378 | 0.038892 | 54.632 | 0.038517 | 54.835 | 0.019413 | 55.058 | 0.019238 | 55.289 |
| 475 | 0.040194 | 58.079 | 0.039441 | 58.227 | 0.033196 | 58.227 | 0.03987 | 58.464 | 0.038536 | 58.732 |

Table 2. Pushover Analysis Results for Effective Cover 30mm

| f_c f_s | 17 | | 18.5 | | 20 | | 21.5 | | 23 | |
|----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|
| | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) |
| 350 | 0.018544 | 42.695 | 0.018336 | 42.843 | 0.01814 | 42.933 | 0.018093 | 42.823 | 0.017949 | 42.842 |
| 380 | 0.019015 | 46.248 | 0.018779 | 46.387 | 0.018569 | 46.523 | 0.018471 | 46.433 | 0.018319 | 46.58 |
| 415 | 0.038154 | 50.142 | 0.019255 | 50.358 | 0.019055 | 50.594 | 0.018887 | 50.244 | 0.018732 | 50.499 |
| 445 | 0.038943 | 53.591 | 0.038484 | 53.661 | 0.038009 | 53.922 | 0.019248 | 53.551 | 0.01908 | 53.793 |
| 475 | 0.039511 | 57.111 | 0.039213 | 57.265 | 0.038742 | 57.416 | 0.038542 | 56.893 | 0.020632 | 57.117 |

Table 3. Pushover Analysis Results for Effective Cover 35mm

| f_c f_s | 17 | | 18.5 | | 20 | | 21.5 | | 23 | |
|----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|
| | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) | Disp (m) | Base Shear (kN) |
| 350 | 0.018417 | 41.451 | 0.018193 | 41.755 | 0.018 | 41.863 | 0.017856 | 42.182 | 0.017708 | 42.398 |
| 380 | 0.0188 | 44.713 | 0.018593 | 44.979 | 0.018438 | 45.181 | 0.01824 | 45.431 | 0.018108 | 45.813 |
| 415 | 0.019436 | 48.478 | 0.019427 | 48.73 | 0.01884 | 48.959 | 0.018686 | 49.215 | 0.018543 | 49.475 |
| 445 | 0.037523 | 51.807 | 0.03696 | 51.941 | 0.019284 | 52.188 | 0.019184 | 52.506 | 0.019027 | 52.759 |
| 475 | 0.038878 | 55.236 | 0.03765 | 55.414 | 0.037534 | 55.617 | 0.03696 | 55.777 | 0.019634 | 55.999 |

For the effective cover of 30mm and strength of concrete as M17, the displacement varies from 0.018544m to 0.039511m with 15% variation in steel strength and the corresponding base shears are 42.695kN and 57.111kN respectively. It has been discovered from the table that there's significant modification in displacement and base shear for varied strength of the steel however there's a negligible modification discovered for varied concrete strengths. This continues in an exceedingly similar pattern for little changes with the cover to reinforcement. Thus it's been thought-about that the probable modification in acquirement with relation to cover to the reinforcement features a terribly tiny role with respect to displacement and strength. Figure 2 which shows the pushover curves for material variations shows the variations in steel strength has a major effect on push over results of the frame whereas the concrete grade has negligible effect.

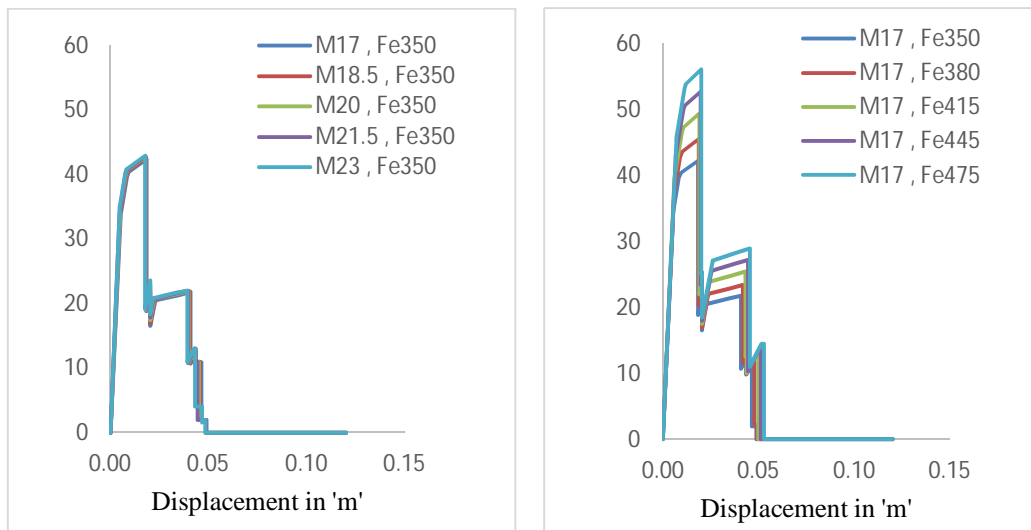


Figure 2. Pushover curves for material variations for the effective cover of 25mm

Effect of plastic hinge formation sequence on pushover analysis results

Pushover analysis necessarily being an exercise to trace structural behavior and understand load deformation characteristics, stiffness degradation, ductility and deformation accommodation consideration of hinge formation sequence and its influence on analysis results is of prime importance. Due to uncertainties in material strength and tolerances in detailing many hinge formation sequences are possible leading to a set of pushover curves.

The frame in figure 1 has been investigated by modelling beams and columns as assemblages of 12 finite elements each and to generate different hinge sequences, weaker elements have been deliberately created at potential plastic hinge locations. To show the influence of sequence of plastic hinge formation on base shear and displacements, the pushover analysis results for first 6 sequences are presented as shown in table 4.

Table 4. Pushover analysis results for sequence variations

| SI No | Sequence series | Base Shear (kN) | Displacement (m) |
|-------|-----------------|-----------------|------------------|
| 1 | 1432 | 48.992 | 0.050238 |
| 2 | 1423 | 45.314 | 0.047463 |
| 3 | 1243 | 36.402 | 0.015835 |
| 4 | 1324 | 35.462 | 0.013686 |
| 5 | 1342 | 35.529 | 0.013701 |
| 6 | 1234 | 30.426 | 0.015663 |

It can be observed that the displacement and base shear varies for every sequence of hinge formation. The minimum displacement obtained is 0.013686m and the corresponding base shear is 35.462kN for hinge sequence 1324 and maximum displacement is 0.050238m with base shear of 48.992kN for hinge sequence 1432. Figure 3 shows pushover curves for all the 6 sequence of hinge formations. The pushover analysis results obtained from all different sequences of hinge formations have the displacement values between these ranges, and that they are all distinctive. This clearly indicates the influence of sequence of hinge formation on pushover analysis results, particularly on displacement characteristics. It's additionally determined that the bottom shear variations are freelance of changes in displacement characteristics. Observations are reliable with assumptions in plastic theory and style, whereby collapse load is invariant to hinge formation sequence. One amongst the doable reasons for variations in base shear results is attributable to the strength parameter variations.

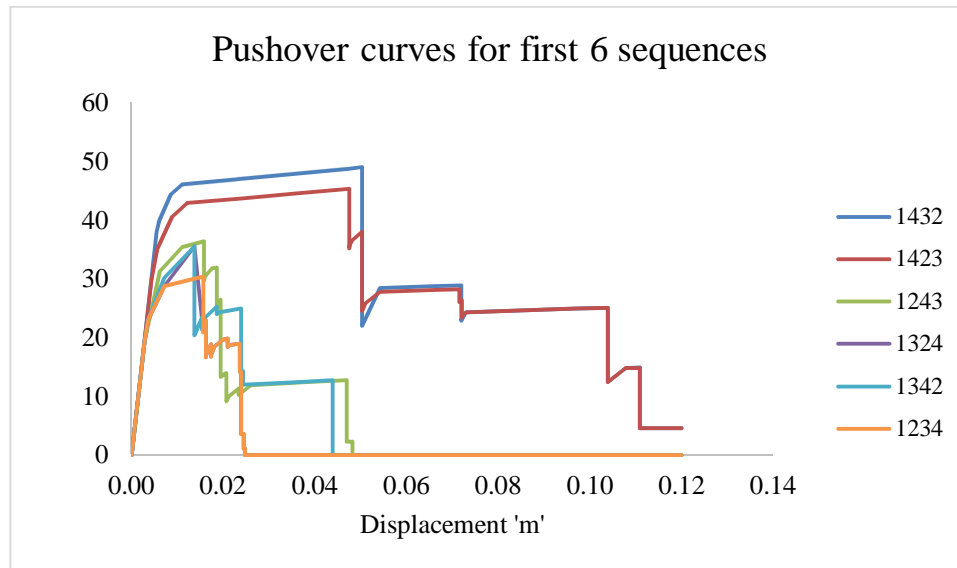


Figure 3. Pushover curves for first 6 sequences

Conclusions

Variations in strength characteristics of material and quality of workmanship quantifiable in terms of errors in dimensions of structural elements and reinforcement placement alters pushover analysis results. As has been illustrated variation of plus or minus 15% in strengths, base shear ranges in + 15%. This is expected as the sections are all under reinforced and as the variation in cover is very limited, variation in strengths are also insignificant. The range of variation in displacements is very significant being -5% to +110% indicating modelling techniques should address by inclusion of these uncertainties. Investigations on influence of hinge formation sequence on analysis results clearly indicate that changes in displacement can be to the tune of +267% due to uncertainties in material quality and workmanship (while base shear shows an increase of 38%). This is too significant, hence can never be ignored. More realistic evaluation of performance becomes possible only when sequence of plastic hinge formation issue is considered and addressed.

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